

# CFD study on high-pressure water-spray cleaning system for CSP mirrors

ASTRI

AUSTRALIAN SOLAR THERMAL RESEARCH INITIATIVE

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## Introduction

This study outlines that the effectiveness of water-jet cleaning processes depends on parameters such as nozzle diameter, jet impingement angle, standoff distance, water velocity and nozzle pressure [1, 2]. Findings shows that the presence of jet rebounds due to the interaction of adjacent flows affect the cleaning ability of the central nozzle in some scenarios. Finally, the CFD model proposed in this analysis has been validated with empirical data from literature.

## Methodology

Two domains have been created to model the water-spray cleaning systems equipped with an interface on points of contact between nozzles and control volume. An inhomogeneous multiphase problem approach has been considered to model the two phase gas-liquid flows. Water at 25°C has been treated as dispersed fluid with droplet size of 10µm while air as a continuous medium at ambient temperature. The continuity and momentum equations describes the state of any type of flow are reported down below, respectively.

$$\frac{\partial p}{\partial t} + \nabla \cdot (\rho u) = 0 \tag{1}$$

$$\frac{\partial \rho u}{\partial t} + \nabla \cdot (\rho u u) = -\nabla p + \nabla \cdot \tau + \rho g \tag{2}$$

Nozzles chosen for this study are full cone convergent types 54mm long with inlet internal diameter of 8mm and outlet internal diameter of 2mm. The contraction has been modeled with an angle set to 22.5 respect to the axis of symmetry (Figure 1). Nozzle interaxial distance has been set to 60mm to minimise interaction between adjacent flows.

Regarding the mesh phase, tetrahedral elements were applied throughout the entire domain with a refinement on grid resolution with minimum size of 0.001 mm, maximum size and maximum facet size of 1mm (Figure 2,3). The mesh resolution generated on the target surface, provides a mesh independent result for the shear stress produced.

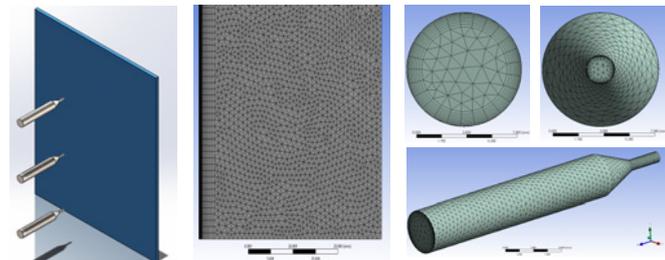


Figure 1: 3D model of the water-spray cleaning system. Figure 2: Control Volume patch conforming mesh with tetrahedrons. Inflation applied close to the wall. Figure 3: Patch conforming mesh with tetrahedral elements with inflation applied on inlet and outlet of nozzles.

## Results

Results confirm an increase in shear force magnitude as a function of increasing inlet pressure. In figure 4, the water-spray behavior impinging normally onto the flat target with three different standoff distances is shown. For low inlet pressures, there is not much difference in the shear force peak. More significant differences occur above 20 Pa of inlet pressure, especially between 5D and 25D standoff.

The shear forces are increased by tilting the jet 15° from the normal (angle of impingement  $\vartheta=75^\circ$ ) (Figure 5). The tilt effect prevents adjacent flows of the outermost nozzles from obstructing the central flow with a subsequent generation of a higher shear stress peak registered than in the normal impingement (Figure 6 and 7). The increase is most marked for the 5D standoff distance with modest enhancement of 3% and 10% for 15D and 25, respectively. The turbulence due to back flows is strongly influenced by the amount of spread of the jet prior to striking the planar surface. At closer standoff distances the jet impingement is more concentrated than for larger standoff, and interaction between jets more less significant.

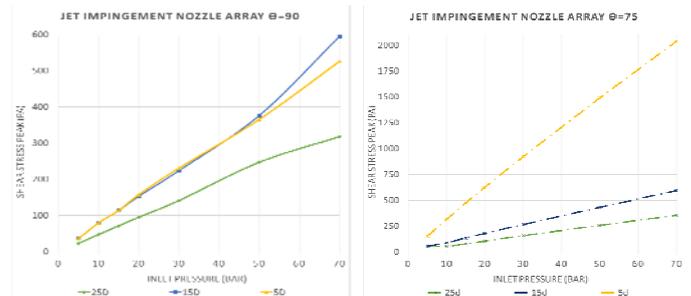


Figure 4: Shear stress generated by nozzles array with  $\vartheta=90^\circ$ . Figure 5: Shear stress generated by the nozzles array with  $\vartheta=75^\circ$ .

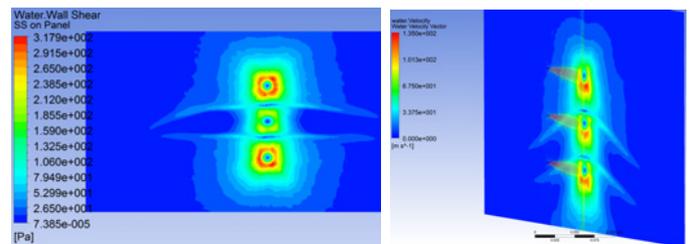


Figure 6: Water Velocity contour of three adjacent jets tilted 15° from the normal. Figure 7: Three adjacent jets tilted 15° from the normal. The non-uniformity of shear flow could adversely affect cleaning.

## Validation

The following CFD model has been compared with empirical experiments conducted by Young et al. (Figure 8). Moreover, we conducted a dimensionless analysis to compare our findings with Smedley's experimental results (Figure 9).

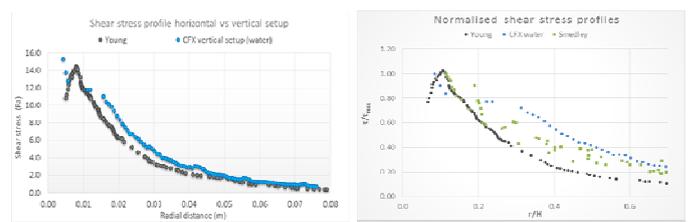


Figure 8: Model validation with Young's experimental data. Figure 9: Dimensionless model validation.

## Conclusions

In this study a detailed analysis of water-jet impingement on a flat surface has been performed with multiple nozzle configuration in line. Three different standoff distances in conjunction with the variation of inlet pressure and angle of impingement have been considered in the CFD simulations with ANSYS v15 software.

Findings confirm a significant increase of shear stress as the standoff distance decreases. By varying the angle of impingement from  $\vartheta=90^\circ$  to  $\vartheta=75^\circ$  for both configurations, an enhancement of shear forces occurs for all standoff distances but is more effective at 5D. Fluid flow and fluid shear may be significantly disrupted due to interaction between adjacent jets. Varying the angle of impingement indeed from  $\vartheta=90^\circ$  to  $\vartheta=75^\circ$ , an enhancement of shear forces occurs for all standoff distances with discontinuance of back flows.

Nozzle design and arrangement should minimise turbulent flow in order to maximise cleaning efficiency.



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- REFERENCES**
1. M. C. Leu, P. Meng, E. S. Geskin, and L. Tismenesky, "Mathematical modeling and experimental verification of stationary waterjet cleaning process," Journal of Manufacturing Science and Engineering, Transactions of the ASME, vol. 120, pp. 571-579, 1998
  2. A. Guha, R. M. Barron, and R. Balachandrar, "An experimental and numerical study of water jet cleaning process," Journal of Materials Processing Technology, vol. 211, pp. 610-618, 4/1/ 2011

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